

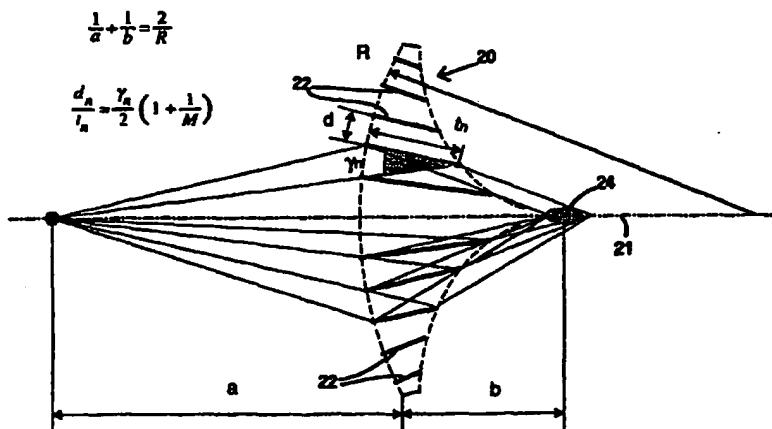
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(54) Title: LENSES FORMED BY ARRAYS OF REFLECTORS



$$\frac{d_n}{t_n} = \frac{\gamma_n}{2} \left(1 + \frac{1}{M} \right) \quad (a)$$

(57) Abstract

A lens, suitable for directing radiation, comprising an array of planar reflecting elements or slats (12, 22). Each reflecting element (12, 22) is of non-uniform extent or surface area t (Figure 1), and/or is non-uniformly spacing d from adjacent elements (Figure 2). The elements may be parallel (Figures 1 and 2) or non-parallel (Figure 3). Each element (12, 22) is positioned such that the ratio of spacing d_n to extent t_n is determined by the angle of incidence on the n th element γ_n , as is given by the relationship (a) where d_n is the spacing between the n th and $(n+1)$ th adjacent elements of the lens, t_n is the length of the n th element, and M is the magnification of the lens.

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LENSES FORMED BY ARRAYS OF REFLECTORS

Technical Field

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This invention concerns optical elements for use as lenses, collimators and collectors of radiation. More particularly, it concerns lenses formed by arrays of reflecting slats, which are suitable for focusing, collimating, or collecting radiation.

10 Background to the invention

The specification of International patent application No PCT/AU93/00453 discloses a range of radiation control devices (including radiation deflectors, concentrators and lenses), each of which is formed by an array of substantially identical reflecting elements. In addition, it is noted in the specification of International patent application No PCT/AU93/00453 that an array of elongate reflectors can be used for one-dimensional focusing (line focusing) of radiation, and that two such arrays of reflectors, crossed at right angles, will form the equivalent of an array of reflecting channels, with each channel having a rectangular cross-section (which is a square cross-section when the reflectors of each array of parallel reflectors have the same spacing). Thus a two-dimensional focusing array or lens can be constructed using two arrays of reflector strips or slats.

One advantage possessed by optical devices formed by an array of reflecting slats - including the "90° crossed-slats" lens referred to above - is that the surfaces of the elongate reflectors can be polished and examined for flaws before the arrays of reflectors are assembled to form the optical device. This feature, as also noted in the specification of International patent application No PCT/AU93/00453, permits the reflective surfaces of the slats to be coated in a manner which ensures that those surfaces are selectively reflective at predetermined wavelengths.

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The present inventor has also shown that this type of 90° crossed-slats lens has an additional advantage over the devices previously used to focus x-radiation (and other

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radiation having a wave-like character) onto a focal zone. The additional advantage is a significant increase in the "intensity gain" of the lens or focusing device. In this field, the gain, G, of a lens or focusing device is defined by the relationship:

$$G = \frac{I_d}{I_o}$$

where I_d is the intensity of radiation in the focal spot or zone of the device and I_o is the
5 intensity of radiation at the same location in the absence of the focusing device.

Disclosure of the present invention

In further developmental work with slatted lenses and crossed-slats lenses, the
10 present inventor has ascertained that improved slatted lenses with a focussing efficiency approaching 100% can be produced if the individual reflectors or slats of the lens are not essentially the same as each other, but the slats have a progressive change in surface area as the distance of the slats from the axis of the lens increases. The lenses are preferably produced such that, (i) the slats are planar, and (ii) the change in surface area of the slats
15 with distance from the axis of the lens will be a decrease in surface area. However, in the manufacture of such lenses, the slats of a lens may conveniently be in groups of equal "front-to-back" length, t , but with varying spacing, d , between the slats in a group, such that the ratio of d_n/t_n is determined by the angle of incidence, on the nth slat of the lens,
20 of radiation from a point source on the lens axis, γ_n , as is approximately given by the relationship:

$$\gamma_n = \frac{d_n}{t_n}$$

for a magnification of one,

and, perhaps more precisely given by:

$$\frac{d_n}{t_n} = \frac{\gamma_n}{2} \left(1 + \frac{1}{M}\right)$$

where d_n is the separation (or spacing) between the nth and (n+l)th slats of the lens, t_n is the extent of the nth slat in a direction parallel to the lens axis, and, M is the

magnification of the lens.

- Preferably, the separation of the slats of the lens (that is, the spacing - or average spacing - between adjacent slats of the lens) will be such that no slat or reflector creates
- 5 a "shadow" on its adjacent outer reflector in the lens, from radiation from a point source at an expected point on the axis of the lens. This usually means that the spacing, d, between adjacent slats will increase progressively with the distance of the slat from the axis of the lens, and the possibility of multiple reflections of radiant energy from that source, in the space between adjacent slats, will be minimised. In the case of a focusing
- 10 lens, this will maximise the energy focused by the lens, which will further increase the gain of the lens.

- Thus, according to the present invention, there is provided an improved slatted lens which comprises a plurality of spaced-apart slats disposed symmetrically about the
- 15 axis of the lens, each slat having one face which is towards the axis of the lens, said one face having a reflective surface, characterised in that the relationship between (i) the length, t, of a slat (ii) the spacing, d, between adjacent slats, and (iii) the angle of incidence, γ , of radiation from a point source on the axis of the lens, for the nth slat from the lens axis, is given by

$$\frac{d_n}{t_n} = \frac{\gamma_n}{2} \left(1 + \frac{1}{M}\right)$$

- 20 Although this definition of the new slatted lens of the present invention requires only one face of each slat to have a reflective surface, in many instances (for example, if the lens is to be used with an extended source of radiation, or for concentrating partially diffused radiation) it will be preferable for both faces of each slat to have a reflective surface.

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The generatrix (i.e. a line normal to each of the reflectors) of a lens with plane reflectors (slats) may have (i) a parabolic shape when the lens is to be used to focus a parallel beam, or to produce a collimated beam from a point source, (ii) an elliptical shape to focus a converging beam, or to produce a diverging beam from a point source,

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or (iii) a hyperbolic shape to focus a diverging beam, particularly a convex hyperbolic shape to achieve a higher intensity gain in the focal spot (demagnification), or a concave hyperbolic shape for magnification. In narrow angle lenses the generatrix will typically have the shape of part of a circular cylinder, as a parabola, a hyperbola or an ellipse all
5 approximate to a circle for small off-axis angles.

If the envelope of the leading edges or the trailing edges of the slats of the slatted lens is substantially a plane which is orthogonal to the axis of the lens, two such slatted lenses may be placed with their substantially planar slat edges closely adjacent to each
10 other (preferably abutting each other) and with their slats "crossed at 90°", to form an improved crossed-slats lens wherein the two one-dimensional lenses have a common centre of curvature. As will be understood to persons skilled in the art, a lens of this type is described above and in the specification of International patent application No PCT/AU93/00453, the details of such specification of which should be considered to be
15 entirely incorporated herein by the reference thereto.

In one broad form, the present invention provides a lens, suitable for directing radiation, comprising an array of planar reflecting elements, characterised in that each of said elements are of non-uniform extent or surface area and/or are non-uniformly spaced
20 from adjacent elements.

Preferably, the surface area of each element decreases relative to adjacent elements, as the distance of each element from an axis of said lens increases.
25 Alternatively, but also preferably the spacing between each element increases as the distance of each element from an axis of said lens increases, whilst the extent of each element remains the same.

In a preferred form, each element is spaced and/or has a surface area such that no
30 element creates a shadow on an adjacent element positioned outwardly thereof.

Preferably, the ratio of d_n/t_n is determined by angle of incidence γ_n of radiation

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on each element of said lens as is given by the relationship:

$$\frac{d_n}{t_n} \approx \gamma_n$$

where d_n is the spacing between the nth and (n+1)th adjacent elements of the lens, and t_n is the length of the nth element.

5 Most preferably, the ratio of d_n/t_n is determined by the angle of incidence γ_n of radiation on each element of said lens as is given by the relationship:

$$\frac{d_n}{t_n} = \frac{\gamma_n}{2} \left(1 + \frac{1}{M}\right)$$

where d_n is the spacing between the nth and (n+1)th adjacent elements of the lens, t_n is the length of the nth element, and M is the magnification of the lens.

10 In a preferred form, either one or both faces of the element is provided with a reflective surface.

Preferably, the generatrix of the lens is of simple or compound, hyperbolic (concave hyperbolic or convex hyperbolic), parabolic, elliptic or circular shape.

15 In a preferred form a cross-slatted lens is formed of two lenses as hereinbefore described, wherein their respective elements are placed with their substantially planar edges closely adjacent to each other (preferably abutting each other) and with their elements 'crossed at 90°', the two lenses having a common centre of curvature.

20 Most preferably, the cross-slatted lens forms an improved cross-slatted lens as disclosed in the specification of PCT/AU93/00453.

25 Preferably, said reflective elements are formed as planar slots in transparent material and whereby reflection is due to total internal reflection.

In an alternatively preferred form, said reflective elements are crystals or multi-

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layer mirrors and reflection is due to Bragg reflection.

In another preferred form, a multi-lens is formed of two lenses as hereinbefore described wherein said multi-lens is used as a beam profile homogeniser to arrange a first type of beam into a second type of beam.

In a preferred embodiment, said lens is utilised as a sky-light enhancer.

In another preferred embodiment, said lens is utilised as a solar concentrator, in the form of a simple or compound hyperbolic shape.

These and other features of the present invention will be better understood from the following description of embodiments of the present invention, which are provided by way of example only. In the following description, reference will be made to the accompanying drawings.

Brief description of the accompanying drawings

Figure 1 is schematic sectional representation of a slatted lens having planar reflectors and having a magnification of 1, constructed in accordance with the present invention;

Figure 2 is a schematic representation of a modified form of the lens of Figure 1;

Figure 3 is a representation, similar to that of Figure 1, of another modified form of the slatted lens shown in Figure 1, having a magnification which is greater than 1 or less than 1 (depending on the way in which the lens is used);

Figure 4(a) is a representation, similar to that of Figure 3, of another modified form of the lens to focus parallel beams, in which the generatrix (i.e. a line normal to each of the reflectors) of a lens with plane reflectors (as in Figure 3) is a parabola;

Figure 4(b) is a representation of another modified form of the lens to focus converging beams, in which the generatrix of the lens with plane reflectors is of elliptical shape;

Figure 4(c) is a representation, of another modified form of the lens to focus

diverging beams, in which the generatrix of the lens with a plane reflectors is a hyperbola;

Figure 4(d) is a representation of another modified form of the lens for magnification, in which the generatrix of the lens with plane reflectors is of concave 5 hyperbolic shape;

Figure 5 illustrates a lens similar to that in Figure 3, but with the reflectors formed as planar slats in a transparent material with refractive index greater than 1, and reflection is due to total internal reflection;

Figure 6 illustrates a lens to focus X-rays similar to that in Figure 3, but wherein 10 the reflectors are crystals or multi-layer mirrors, and reflection is due to Bragg reflection;

Figure 7 illustrates an improved 90° crossed-slats lens formed by two one-dimensional slatted lenses of the types featured in Figures 1 to 3 crossed at right angles, various views being shown in Figures 7(a) to 7(d);

Figure 8 illustrates an example of an array designed as a beam profile 15 homogeniser to arrange a Gaussian beam into a 'top hat' beam;

Figure 9 illustrates a practical application of a lens constructed in accordance with the present invention, embodied as a 2-D sky light enhancer made of blocks of transparent plastics material with slots or reflectors for total internal reflections, Figure 9(a) showing an elevational cross-sectional view thereof, and Figure 9(b) showing a top 20 view thereof;

Figure 10 illustrates an elevational cross-sectional view of a trough-like solar concentrator formed by an array of reflectors which may be formed of parabolic, hyperbolic and/or elliptical shape; and

Figure 11 illustrates, in Figures 11(a) and 11(b) an elevational cross-sectional 25 views of compound hyperbolic concentrators.

Detailed description of the illustrated embodiments

Figure 1 is a sectional view of a slatted lens 10 having a plurality of planar slats 30 12 mounted symmetrically above and below the axis 11 of the lens. The face of each slat 12 which is towards the axis 11 has a reflective surface. The other face of each slat 12 may also have a reflective surface. Normally, each slat 12 will extend the same distance

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in the plane orthogonal to the drawing, as each other slat in the array. A point source 13 of radiation is positioned on the axis of the lens 10. As shown by a series of ray paths, the lens 10 acts to focus radiation from the source 13 onto a focal zone 14, which will be an elongate or line focal zone, extending in a direction orthogonal to the plane of

5 Figure 1.

For the sake of clarity, Figure 1 shows only five reflectors or slats on each side of the lens axis 11. In practice, many more reflective slats will normally be used to produce a slatted lens, particularly if the source 13 is a source of x-rays. A similar 10 comment applies to the illustrated lenses in the other Figures of the accompanying drawings.

It will be noted that in the lens featured in Figure 1, the slats 12 which are closest to the lens axis 11 have a greater surface area than the slats 12 which are remote from 15 the lens axis 11, and that there is a progressive change in the surface area of the slats with the distance of a slat from the lens axis 11. In addition, the spacing between the slats 12 which are remote from the lens axis 11 is greater than the separation of the slats which are adjacent to the lens axis. These dimensional changes are chosen to ensure that (i) all 20 radiation from the source 13 which is incident on the lens 10 is reflected towards the focal zone 14 by a reflective surface of a slat 12 of the lens, and (ii) no radiation from the source 13 is reflected more than once in its passage through a channel between two adjacent slats of the lens. Thus essentially all radiation from the source 13 which is incident upon the slatted lens 10 is directed to the focal zone 14. This maximises the gain 25 of the lens 10.

25

It will be apparent to persons familiar with optical devices that the lens of Figure 1 has a magnification of 1, for the slats of the lens are all parallel to the lens axis 11. Thus a ray from the source 13 which makes an angle α to the lens axis will be reflected once by a slat of the lens and the reflected ray will also make an angle α with the lens 30 axis 11.

Figure 1 illustrates an ideal construction for a slatted lens with a magnification of

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1, with a progressive change in the front-to-back length, t , of the slats as the distance of the slat from the lens axis increases. In practice, when many slats are to be incorporated into the lens, the lens construction shown in Figure 2 will normally be adopted.

- 5 The lens shown schematically in Figure 2 requires slats of three sizes only. The slats are mounted in groups of identical slats. However, the spacing between the slats of each group is varied progressively so that (as in the lens of Figure 1) if the angle of incidence of radiation from the source 13 on the n th slat from the lens axis is γ_n (in practice, because there are many more reflective slats 12 in a practical realisation of the
10 lens shown in Figures 1 and 2, the angle γ_n will not vary significantly over the reflective surface of the n th slat), the ratio d_n/t_n is defined by the relationship:

$$\frac{d_n}{t_n} = \frac{\gamma_n}{2} \left(1 + \frac{1}{M}\right)$$

where d_n is the separation (or spacing) between the n th and $(n+1)$ th slats of the lens, and t_n is the extent of the n th slat in a direction parallel to the lens axis 11.

- 15 The lens 20 shown in Figure 3 is another modified form of the lens of Figure 1. The main modification in this case is the inclination of the planar surfaces of the slats 22 relative to the lens axis 21. For radiation from the source 13, this results in a reduction of the size of the focal zone 24, and a consequential increase in the gain and in the
20 magnification of the lens 20. Clearly, if the source of radiation should be located at 24, and the image produced at 13, the lens would have a magnification of less than 1, although it would still have a high gain.

- Figure 4 shows, in Figures 4(a) to 4(d), representations of arrays, each having a
25 differently shaped generatrix. The generatrix is defined to be the line normal to each of the reflectors. Each of Figures 4(a) to 4(d) display lenses with plane reflectors or slats. Figure 4(a) shows an array wherein the generatrix of the lens is of parabolic shape, to focus a parallel beam, or to produce a collimated beam from a point source. Figure 4(b) shows an array wherein the generatrix of the lens is of elliptical shape, to focus a

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converging beam or to produce a diverging beam from a point source. The generatrix of the lens should be of hyperbolic shape to focus a diverging beam. It should be convex hyperbolic, as shown in Figure 4(c) to achieve a high intensity gain in the focal spot, that is, demagnification, and, it should be concave hyperbolic for magnification, as shown in 5 Figure 4(d). In narrow angle lenses, the generatrix may have the a parabolic, hyperbolic or elliptic shape, which all approximate closely to a circle for small off-axis angles.

Figure 5 illustrates a convenient mechanism for constructing lenses of the type shown in, Figures 1, 3 and 4, when the lenses are to be used with electromagnetic 10 radiation, such as in the visible spectrum or with ultra-violet radiation or infra-red radiation.

The lens of Figure 5 is constructed of optical quality material which is transparent to the radiation with which the lens is to be used. The transparent material must have a 15 refractive index, n , for that radiation, which is greater than 1.

For radiation in the visible spectrum, a number of plastic materials and glasses can be used in this form of lens construction. Slots 80 are cut into a block of the transparent material having the required shape of the slatted lens to be produced. The slots 80 are 20 made at the locations of the slats of the required slatted lens. The slot face which is closest to the axis of the lens must be polished to ensure good lens performance, and for some applications, each face of the slots should be polished (this means that for a lens which is equivalent to a lens having planar slats, the slot faces will be optically flat). The slots 80 need not extend completely through the block of plastic. The front faces 85 and 25 the rear faces 86 of the transparent material between the slots must be optically flat faces for good lens performance.

Figure 5 includes several ray paths from a point source 13 on the lens axis. It will be noted that each off-axis ray is refracted when it strikes the front surface 85 of the 30 optical quality transparent material, and then is reflected (by total internal reflection) from the face of the relevant slot 80, before being refracted again at face 86 on leaving the transparent material of the lens.

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It will be appreciated that slatted lenses, forming arrays of other shapes (such as the lenses shown in Figure 4) may be constructed in this manner, or, by assembling a series of blocks of the optical quality transparent material having (i) a refractive index greater than 1 and (ii) polished surfaces having the required slat shape. Each of the 5 assembled blocks will be spaced from its adjacent block or blocks by a small distance.

Figure 6 illustrates a lens to focus X-rays similar to that in Figure 3, but wherein the reflectors are crystals or multi-layer mirrors, and reflection is Bragg reflection.

10 Various practical applications for the present invention are envisaged by the inventor, as will be described hereafter.

(i) UV, VUV and X-Ray lenses and collimators with high efficiency.

It has been shown that the collection efficiencies of square-channel optics can be 15 increased by modifying the lens structure. Such modifications involve segmenting the plate, or varying channel width, or locally varying the lens thickness.

Figure 7 is an illustrative example of a 90° crossed-slats lens 60 which is constructed using two lenses of the type shown in Figure 3, the two lenses having a 20 common centre of curvature. Such a 90° crossed-slats lens 60 acts to focus incident radiation from a point source to a focal zone. Figure 7(a) shows an elevational view in the y-z plane, Figure 7(b) shows a top view (x-y plane), Figure 7(c) shows an elevational view in the x-z plane, and Figure 7(d) illustrates a three dimensional representation of the lens.

25 A focusing efficiency approaching 100% can be achieved for such a lens with each channel length t_n and channel width d_n , varying as:

$$\frac{d_n}{t_n} = \frac{\gamma_n}{2} \left(1 + \frac{1}{M}\right)$$

where γ_n is the angle between the n-th reflector and the ray entering the n-th channel.

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The focus will be square with a width $M+1$ times the maximum channel width d_n . Therefore to achieve tight focusing and high intensity gain it is worthwhile to vary t_n to satisfy the above condition. 100% efficiency is achieved only for one particular set of source and image distances.

5

(ii) A UV, VUV and X-ray Beam Homogeniser.

Figure 8 shows an example of a double array lens designed as a UV, VUV and X-ray beam profile homogeniser to arrange a Gaussian beam into a 'top hat' beam, for material processing. The requirements are that the surface of the material should be
10 illuminated as uniformly as possible or shaped for intensity according to particular production requirements. An array of optical devices with the ability to manipulate a beam shape has a unique potential to develop a low-cost beam homogeniser with minimal power loss. One of the possible schemes to convert a collimated beam with Gaussian
15 profile in intensity distribution into a focusing beam with homogeneous intensity in a particular sample plane is shown in Figure 8. The first lens is a beam expander (convex parabolic, if the beam is collimated, or hyperbolic in case of diverging beam) and the second is a focusing lens (hyperbolic). To design such a beam homogeniser, it is necessary to take into account the initial beam divergence, near-field distribution,
20 diffraction effects on reflector edges, and the actual beam size to develop the required intensity distribution over the sample.

(iii) Sky light enhancer made of an array of reflectors.

Figure 9 shows, in Figures 9(a) and 9(b), elevational cross-sectional and top views, respectively of a practical application of the arrays of the present invention embodied as
25 a two dimensional sky-light enhancer made of blocks of transparent material, formed of plastics or other material, with slots as reflectors for total internal reflection. A similar configuration could be constructed utilising 'normal' reflectors.

(iv) Elliptical and Hyperbolic array of reflectors for Solar concentrators

30 Figure 10 shows a cross-sectional view of a trough-like solar concentrator, being another practical application of the present invention. The solar concentrator may be made as an array of reflectors with parabolic, hyperbolic or elliptical shape.

(v) Compound hyperbolic concentrators

Figure 11(a) represents an example of an array design as a compound parabolic concentrator. It consists of the right and the left halves which belong to different parabolas, where each parabola focuses the radiation as a parallel beam to the axes of each parabola axis into focal points, both on the absorber. The goal of this design is to maximise the concentration of radiation coming from different angles. The solution is to increase the slope of the axis of the parabolic curve so that extreme rays within the acceptance angle illuminate the absorber within the prescribed dimensions.

Figure 11(b) represents an example of an array design as a compound hyperbolic concentrator. It consists of the right and the left halves which belong to different hyperbolas, where each hyperbola focuses the radiation coming within the acceptance angle into a focal point. The goal of this design is to maximise the concentration of radiation coming within the aperture of the concentrator. The solution is to increase the distance between the axis of the hyperbolic curves so that extreme parallel rays illuminated the absorber within the prescribed dimensions.

It is emphasised that the embodiments of the present invention which are illustrated in the accompanying drawings and described above are only examples of the present invention. Variations of and modifications to the illustrated lenses may be made without departing from the present inventive concept.

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The claims

1. A lens, suitable for directing radiation, comprising an array of planar reflecting elements, characterised in that each of said elements are of non-uniform extent or surface area and/or are non-uniformly spaced from adjacent elements.

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2. A lens as claimed in claim 1, wherein the extent or surface area of each element does not increase relative to adjacent elements, as the distance of each element from an axis of said lens increases.

10 3. A lens as claimed in claim 1, wherein the spacing between adjacent elements increases as the distance of each element from the axis of said lens increases, whilst the extent of each element remains the same.

4. A lens as claimed in any one of claims 1 to 3, wherein the elements are designed
15 and positioned to minimise shadowing on other elements.

5. A lens as claimed in any one of claims 1 to 4, wherein the ratio of d_n/t_n is determined by angle of incidence γ_n of radiation on each element of said lens as is given by the relationship:

$$\frac{d_n}{t_n} = \gamma_n$$

20 where d_n is the spacing between the nth and (n+1)th adjacent elements of the lens, and t_n is the length of the nth element.

25 6. A lens as claimed in any one of claims 1 to 5, wherein the ratio of d_n/t_n is determined by angle of incidence γ_n of radiation on each element of said lens as is given by the relationship:

$$\frac{d_n}{t_n} = \frac{\gamma_n}{2} \left(1 + \frac{1}{M}\right)$$

where d_n is the spacing between the nth and (n+1)th adjacent elements of the lens, t_n is the length of the nth element, and M is the magnification of the lens.

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7. A lens as claimed in any one of claims 1 to 6, wherein either one or both faces of the element is provided with a reflective surface.
8. A lens as claimed in any one of claims 1 to 7, wherein the generatrix of the lens 5 is of simple or compound, hyperbolic, parabolic, elliptical or circular shape.
9. A cross-slatted lens, formed of two lenses as claimed in any one of claims 1 to 8, wherein their respective elements are placed with their substantially planar edges closely adjacent to each other (preferably abutting each other) and with their elements 10 'crossed at 90°, the two lenses having a common centre of curvature.
10. A cross-slatted lens as claimed in claim 9, forming an improved cross-slatted lens as disclosed in the specification of PCT/AU93/00453.
- 15 11. A lens as claimed in any one of claims 1 to 10, wherein said reflective elements are formed as planar slots in transparent material and whereby reflection is due to total internal reflection.
12. A lens as claimed in any one of claims 1 to 10, wherein said reflective elements 20 are crystals or multi-layer mirrors and reflection is due to Bragg reflection.
13. A multi-lens formed of two lenses as claimed in any one of claims 1 to 12, wherein said multi-lens is used as a beam profile homogeniser to arrange a first type of beam into a second type of beam.
- 25 14. A lens as claimed in any one of claims 1 to 13, wherein said lens is utilised as a sky-light enhancer.
15. A lens as claimed in any one of claims 1 to 14, wherein said lens is utilised as a 30 solar concentrator.
16. A lens, substantially as herein described with reference to the accompanying

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drawings.

17. A method of directing radiation utilising an array of reflecting elements, substantially as hereinbefore described.

5

AMENDED CLAIMS

[received by the International Bureau on 16 October 1995 (16.10.95);
 original claim 5 cancelled; original claims 1-4 and 6-17 amended;
 original claims 2-4, 6 and 7-17 renumbered as claims 3-5, 2 and 6-16 (3 pages)]

1. A lens, suitable for directing radiation, comprising an array of planar reflecting elements, characterised in that each of said elements are of non-uniform extent or surface area and/or are non-uniformly spaced from adjacent elements, and further characterised in that the ratio of d_n/t_n is determined by angle of incidence γ_n of radiation on each element of said lens as is given by the relationship:

$$\frac{d_n}{t_n} = \gamma_n$$

where d_n is the spacing between the nth and (n+1)th adjacent elements of the lens, and t_n is the length of the nth element.

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2. A lens as claimed in claim 1, wherein the ratio of d_n/t_n is determined by angle of incidence γ_n of radiation on each element of said lens as is given by the relationship:

$$\frac{d_n}{t_n} = \frac{\gamma_n}{2} \left(1 + \frac{1}{M}\right)$$

where d_n is the spacing between the nth and (n+1)th adjacent elements of the lens, t_n is the length of the nth element, and M is the magnification of the lens.

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3. A lens as claimed in claims 1 or 2, wherein the extent or surface area of each element does not increase relative to adjacent elements, as the distance of each element from an axis of said lens increases.

- 20 4. A lens as claimed in claims 1 or 2, wherein the spacing between adjacent elements increases as the distance of each element from the axis of said lens increases, whilst the extent of each element remains the same.

- 25 5. A lens as claimed in any one of claims 1 to 4, wherein the elements are designed and positioned to minimise shadowing on other elements.

6. A lens as claimed in any one of claims 1 to 5, wherein either one or both faces

of the element is provided with a reflective surface.

7. A lens as claimed in any one of claims 1 to 6, wherein the generatrix of the lens is of simple or compound, hyperbolic, parabolic, elliptical or circular shape.

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8. A cross-slatted lens, formed of two lenses as claimed in any one of claims 1 to 7, wherein their respective elements are placed with their substantially planar edges closely adjacent to each other (preferably abutting each other) and with their elements 'crossed at 90°'.

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9. A cross-slatted lens as claimed in claim 8, forming an improved cross-slatted lens as disclosed in the specification of PCT/AU93/00453.

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10. A lens as claimed in any one of claims 1 to 9, wherein said reflective elements are formed as planar slots in transparent material and whereby reflection is due to total internal reflection.

11. A lens as claimed in any one of claims 1 to 9, wherein said reflective elements are crystals or multi-layer mirrors and reflection is due to Bragg reflection.

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12. A multi-lens formed of two lenses as claimed in any one of claims 1 to 11, wherein said multi-lens is used as a beam profile homogeniser to arrange a first type of beam into a second type of beam.

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13. A lens as claimed in any one of claims 1 to 12, wherein said lens is utilised as a sky-light enhancer.

14. A lens as claimed in any one of claims 1 to 13, wherein said lens is utilised as a solar concentrator.

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15. A lens, substantially as herein described with reference to the accompanying drawings.

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16. A method of directing radiation utilising an array of reflecting elements, substantially as hereinbefore described.

-20-

STATEMENT UNDER ARTICLE 19

Delete the set of claims presently on file and insert the new set of claims attached hereto. New claim 1 incorporates the definition of old claim 5. Old claim 6 is renumbered as new claim 2, and the remaining claims have been renumbered consecutively and had their dependencies altered.

- 1/12 -

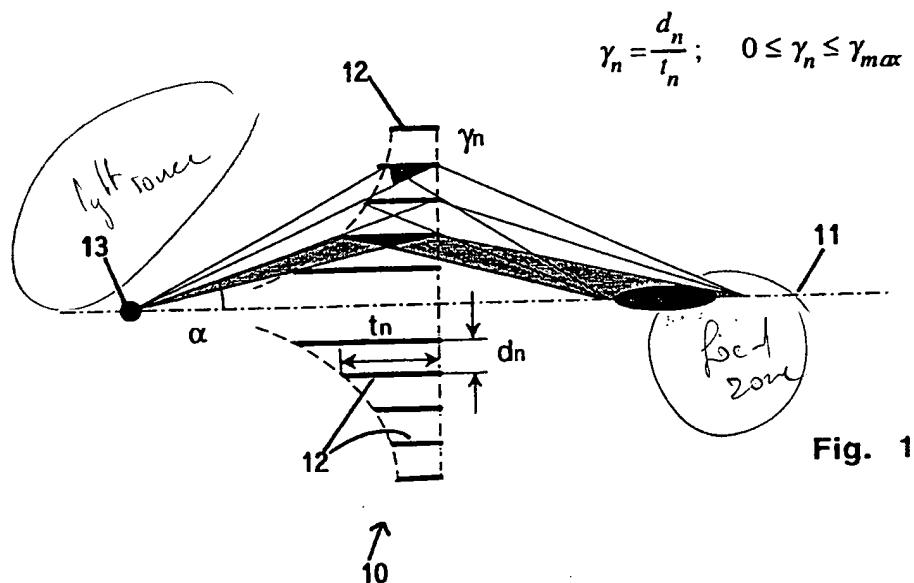


Fig. 1

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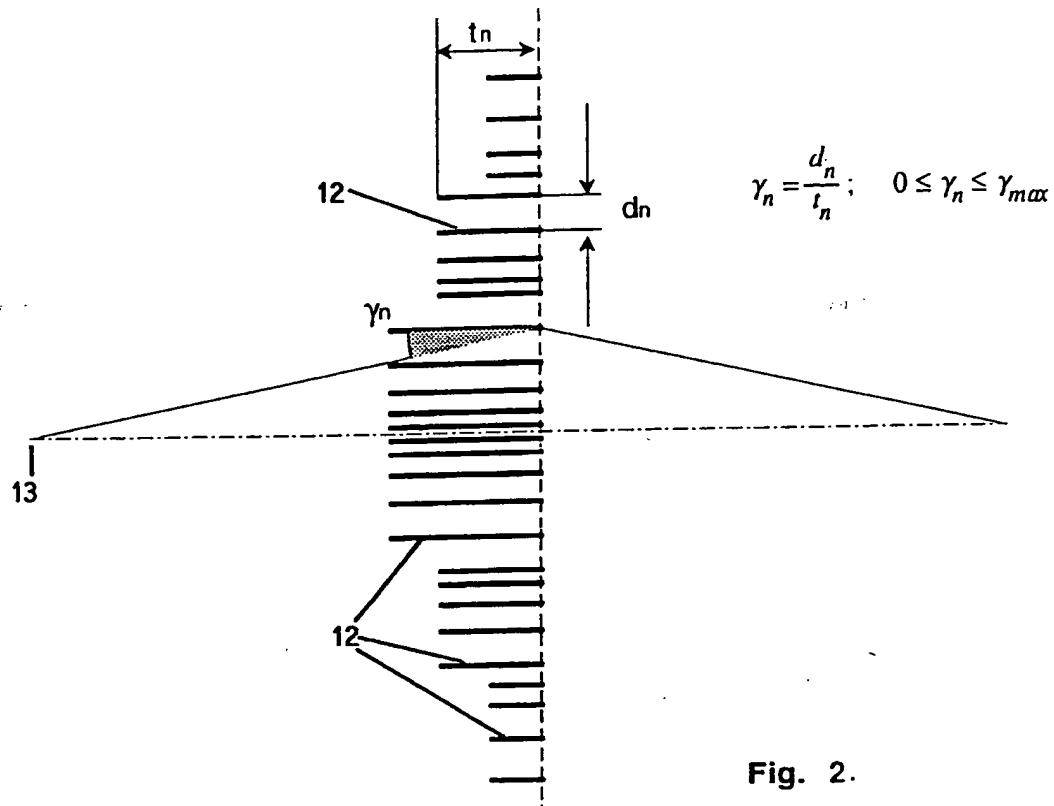


Fig. 2.

- 3/12 -

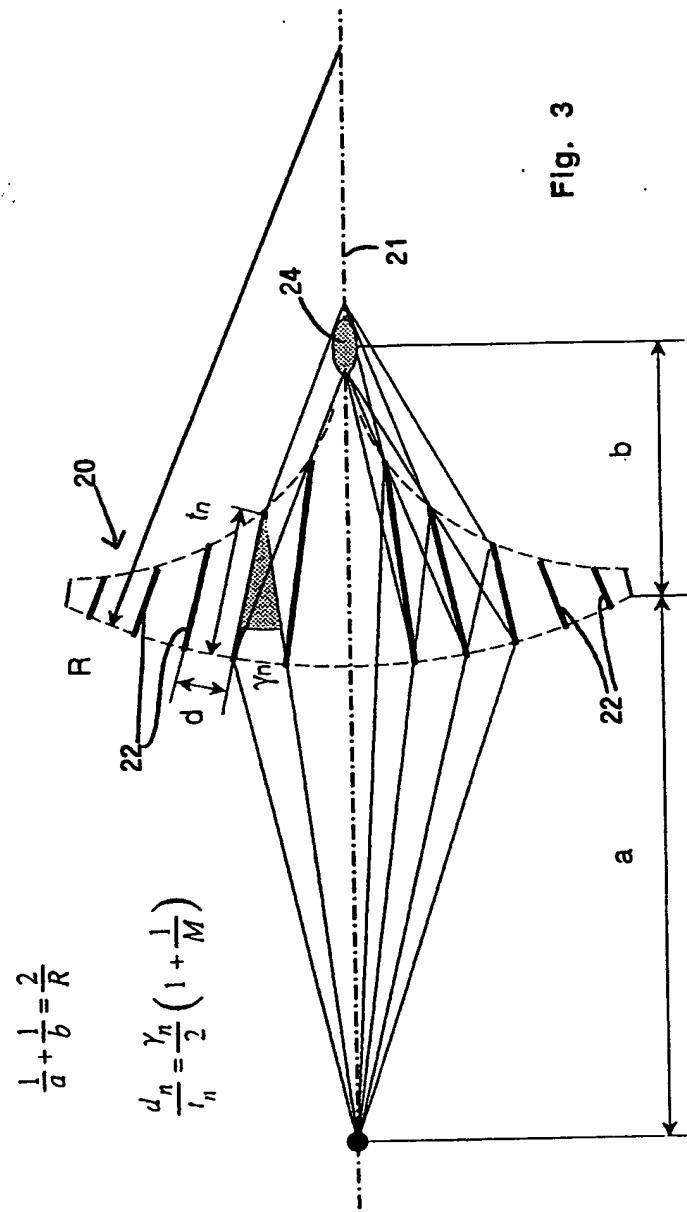


Fig. 3

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Fig. 4b

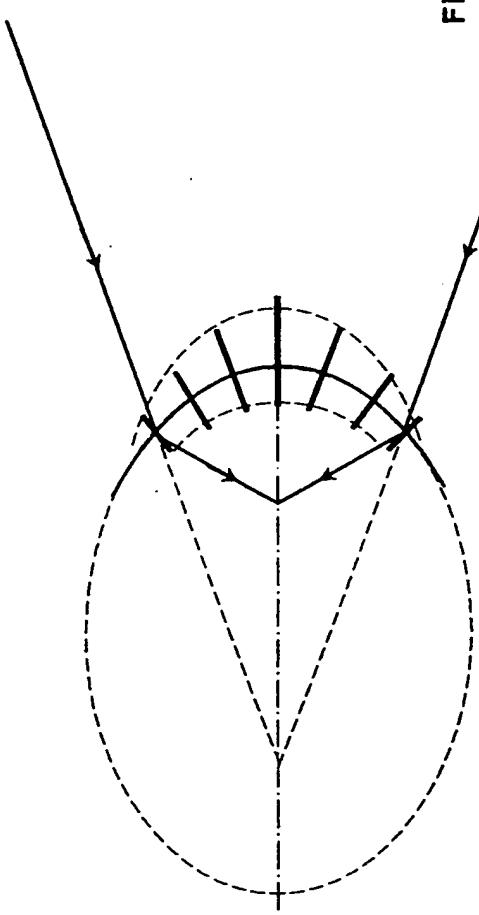


Fig. 4a

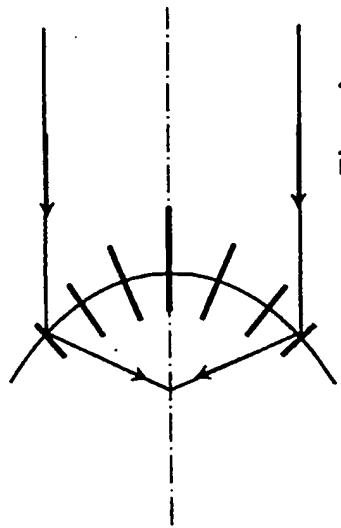


FIG. 4

Fig. 4d

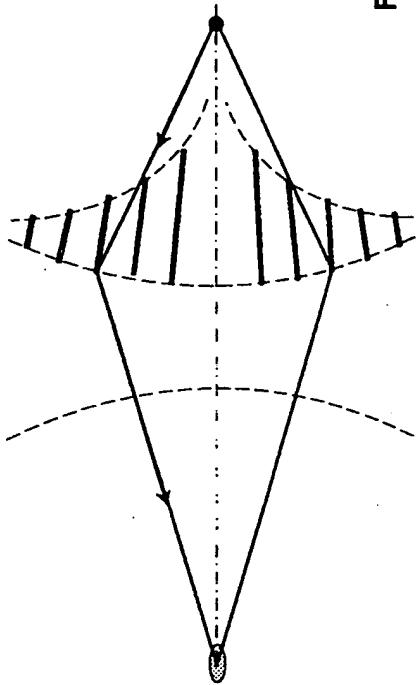
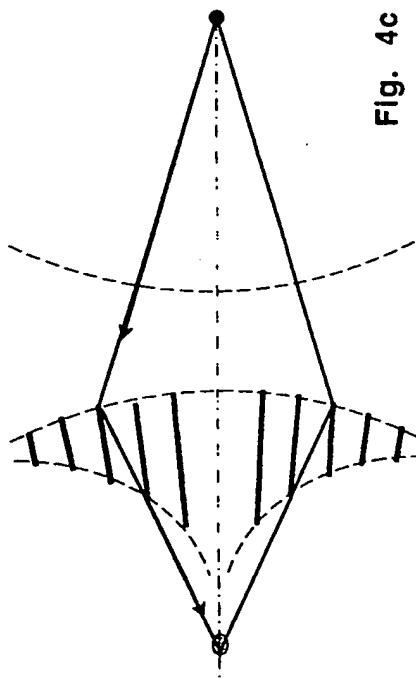
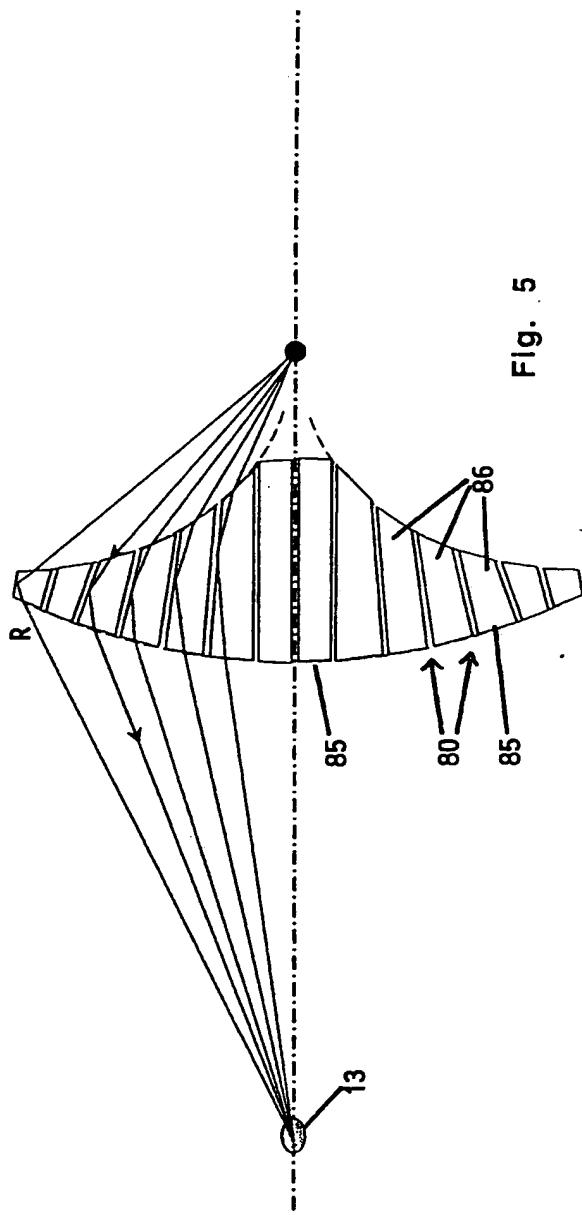


Fig. 4c



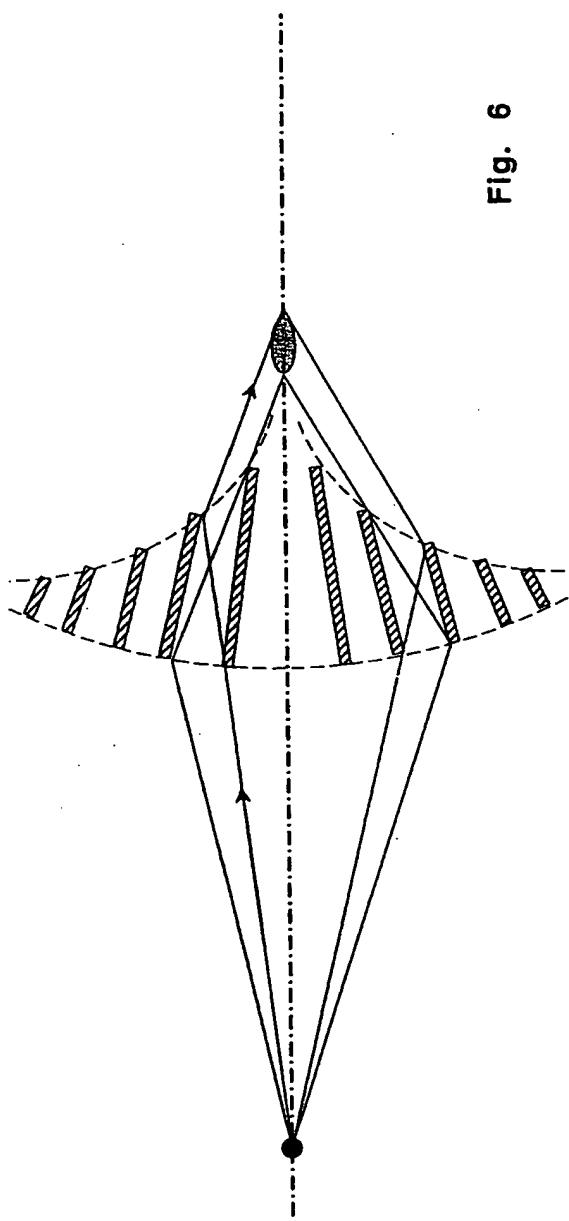
- 5/12 -

Fig. 5



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Fig. 6



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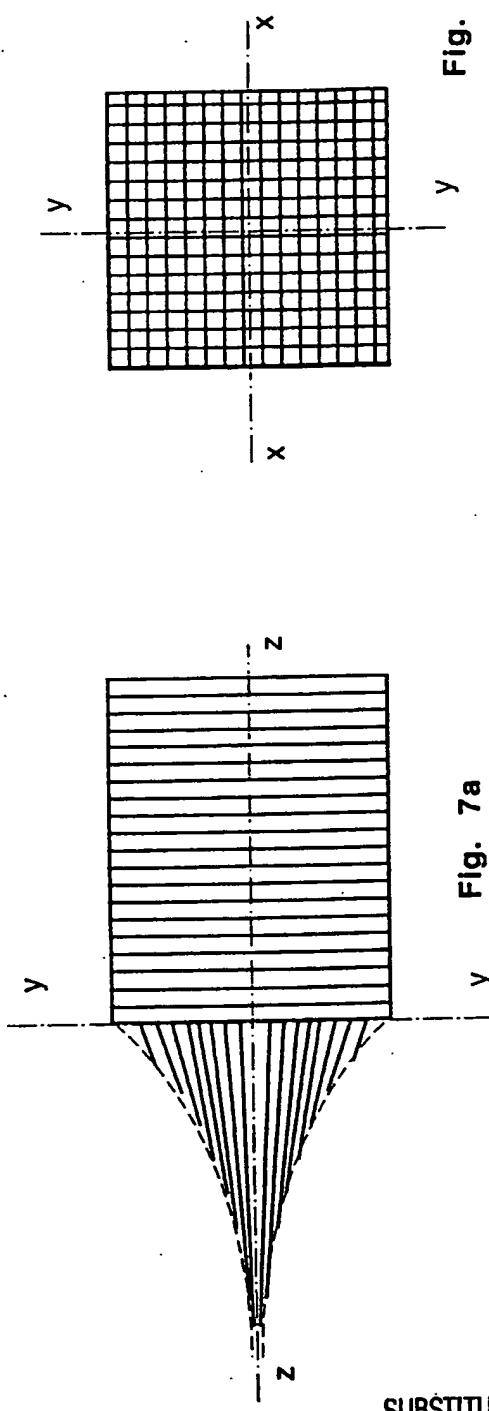


Fig. 7b

SUBSTITUTE SHEET (RULE 26)

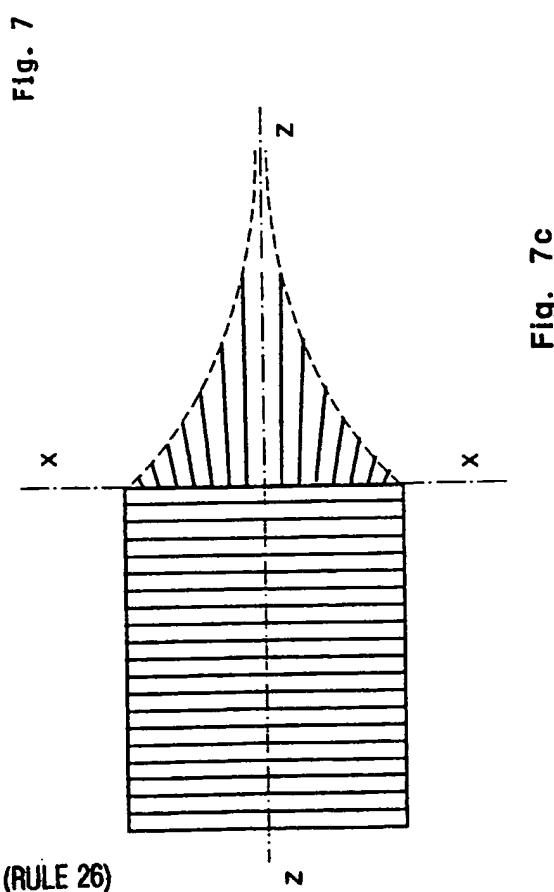


Fig. 7c

Fig. 7d

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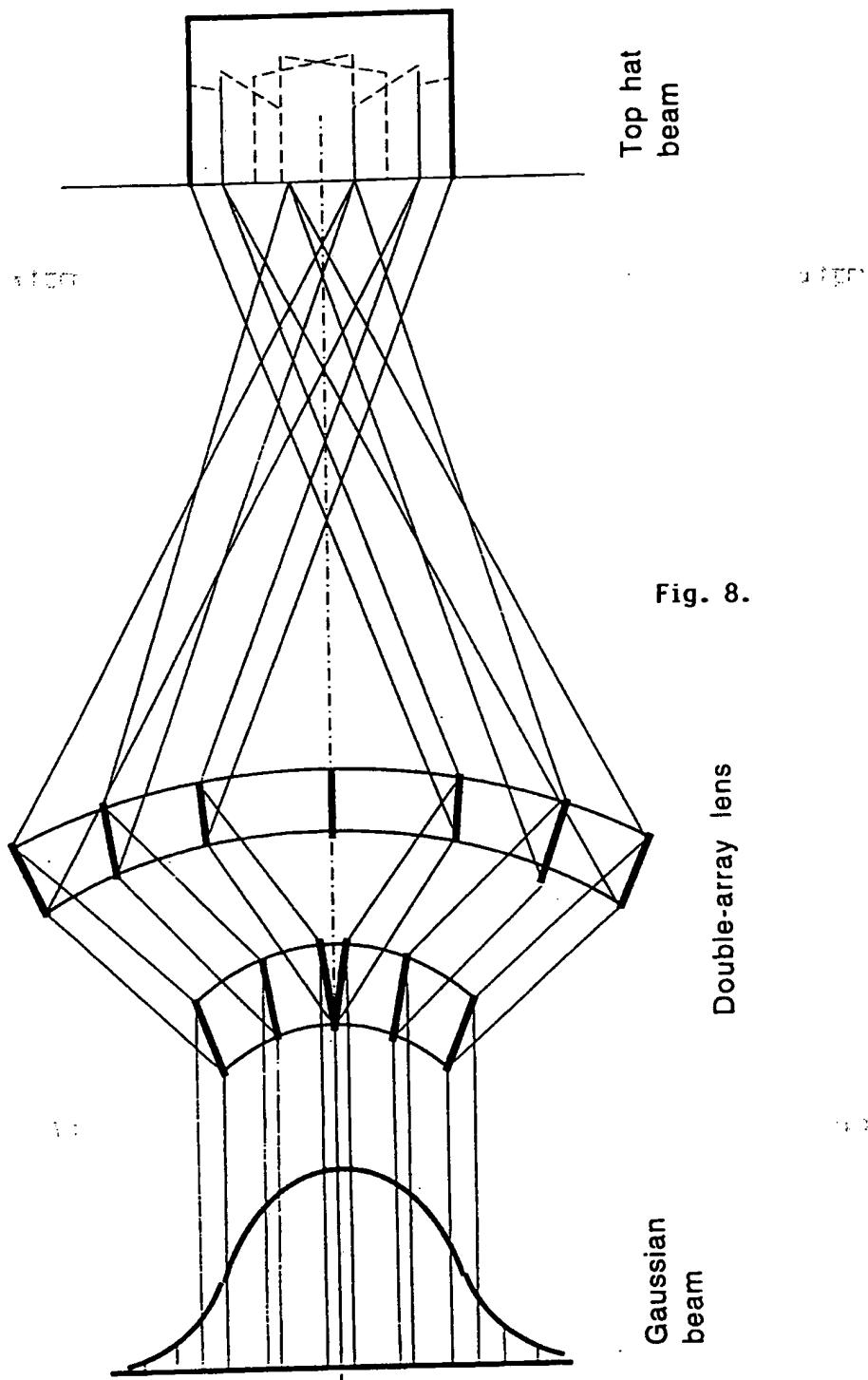
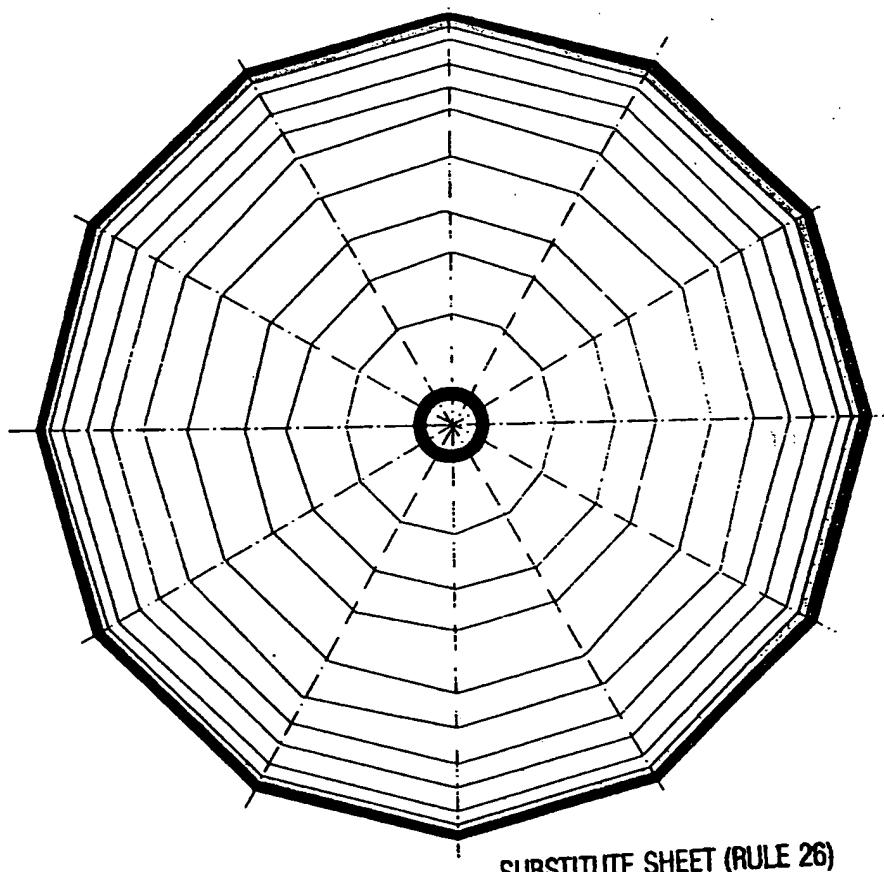
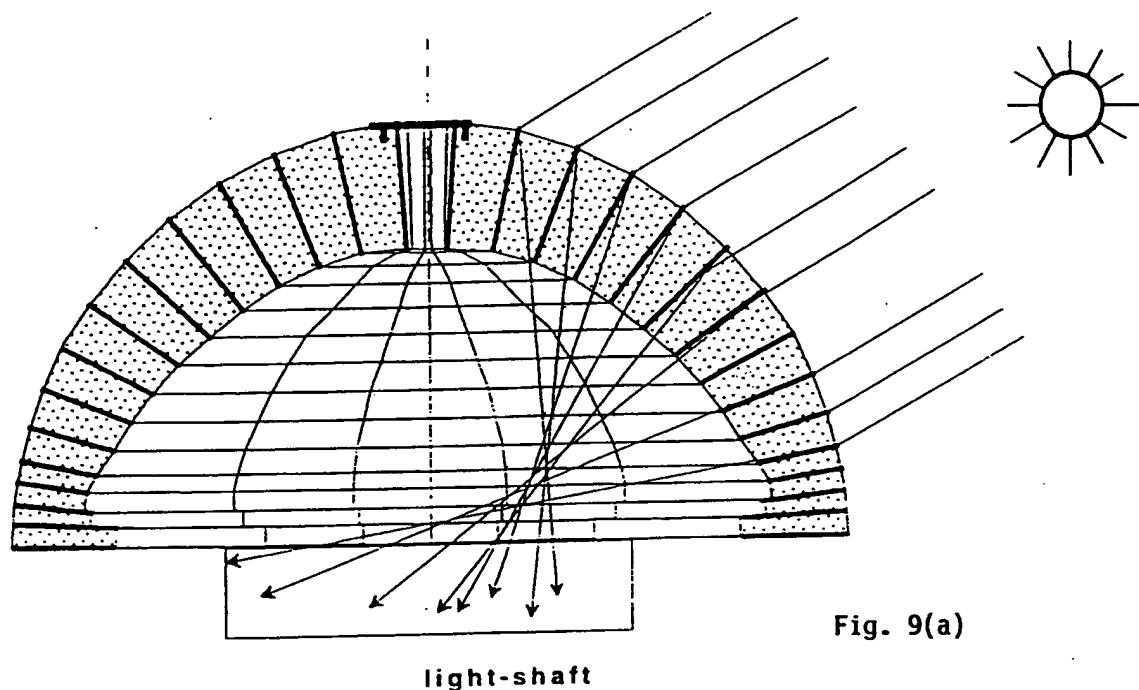


Fig. 8.

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- 10/12 -

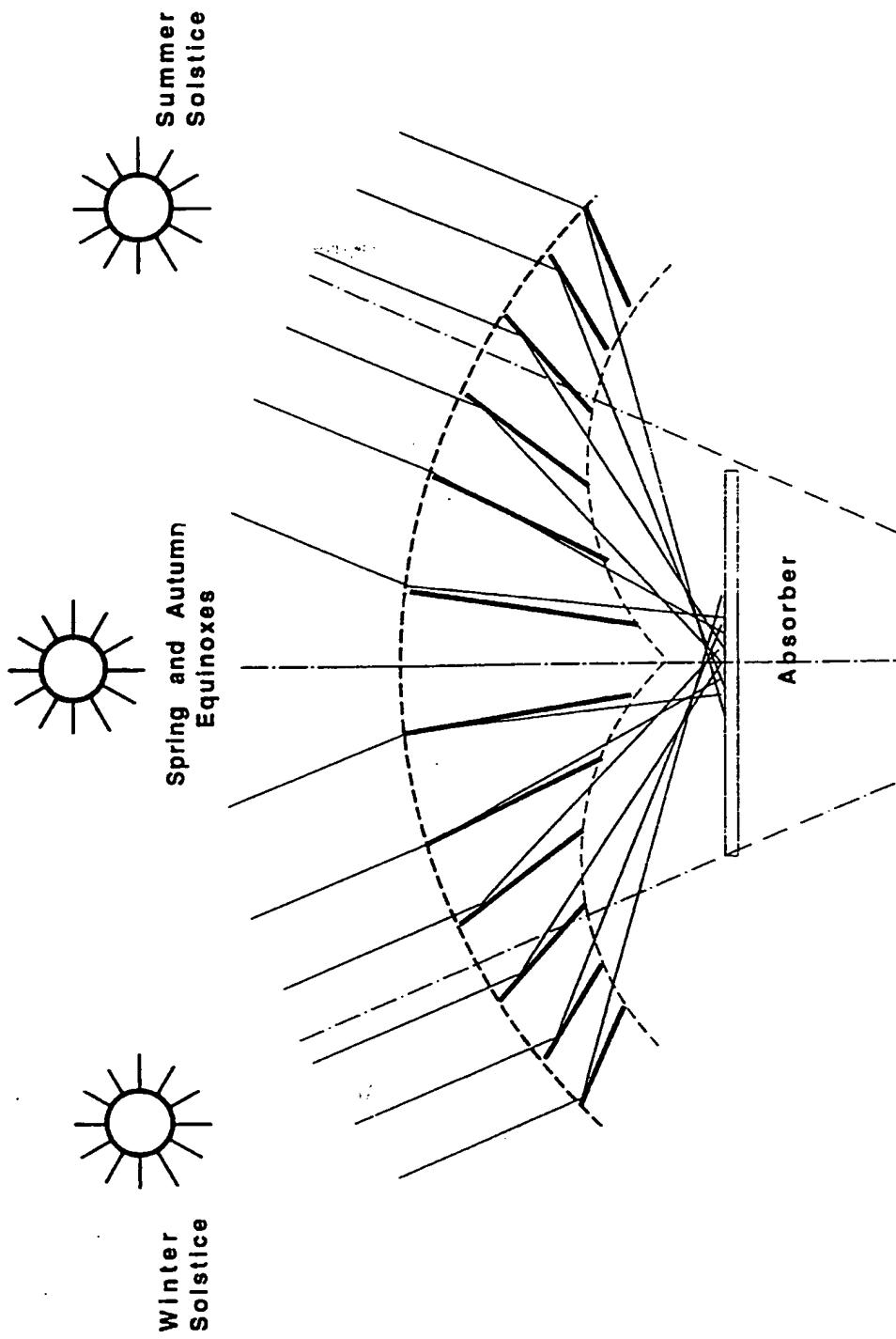
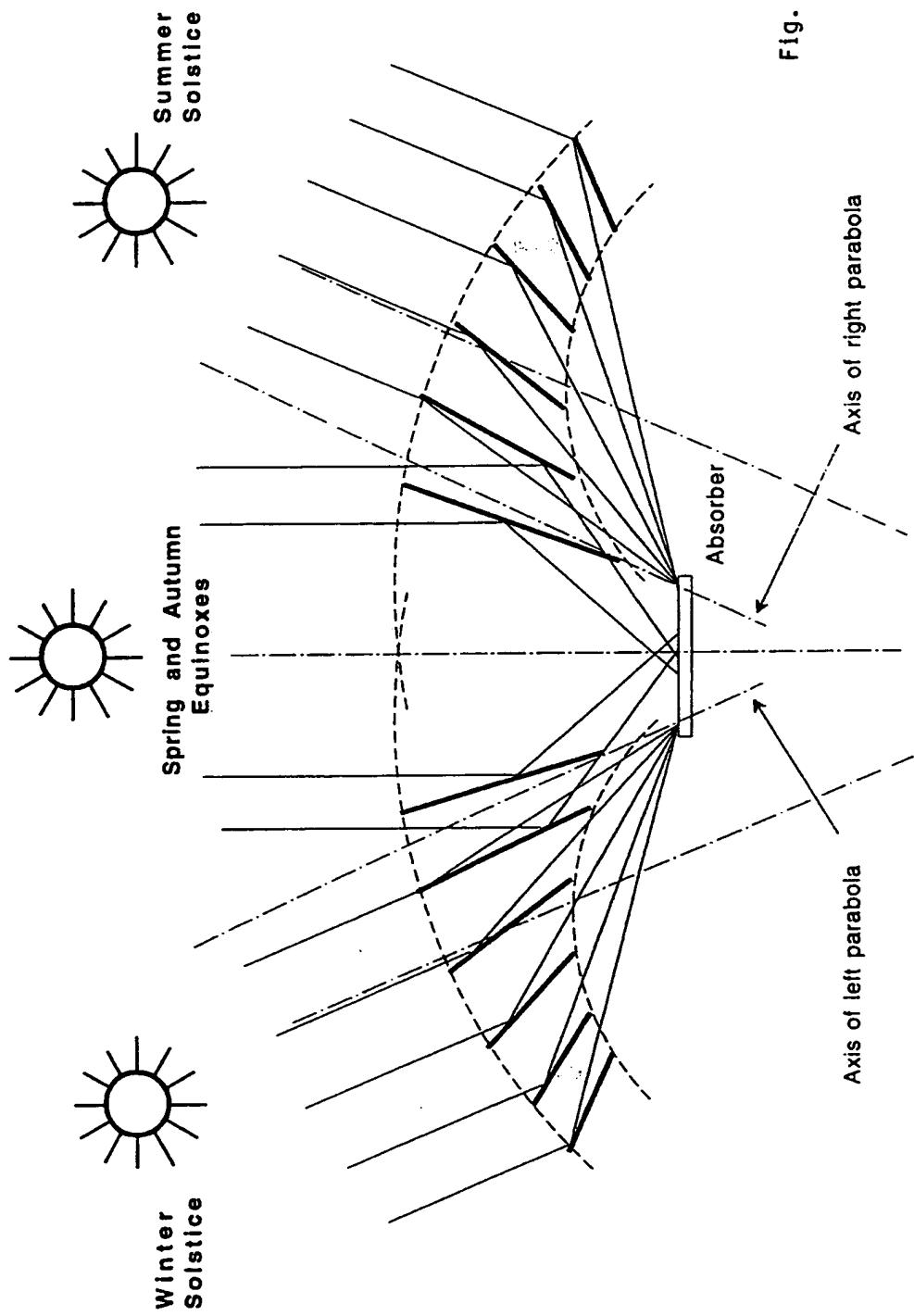


Fig. 10.

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- 12/12 -

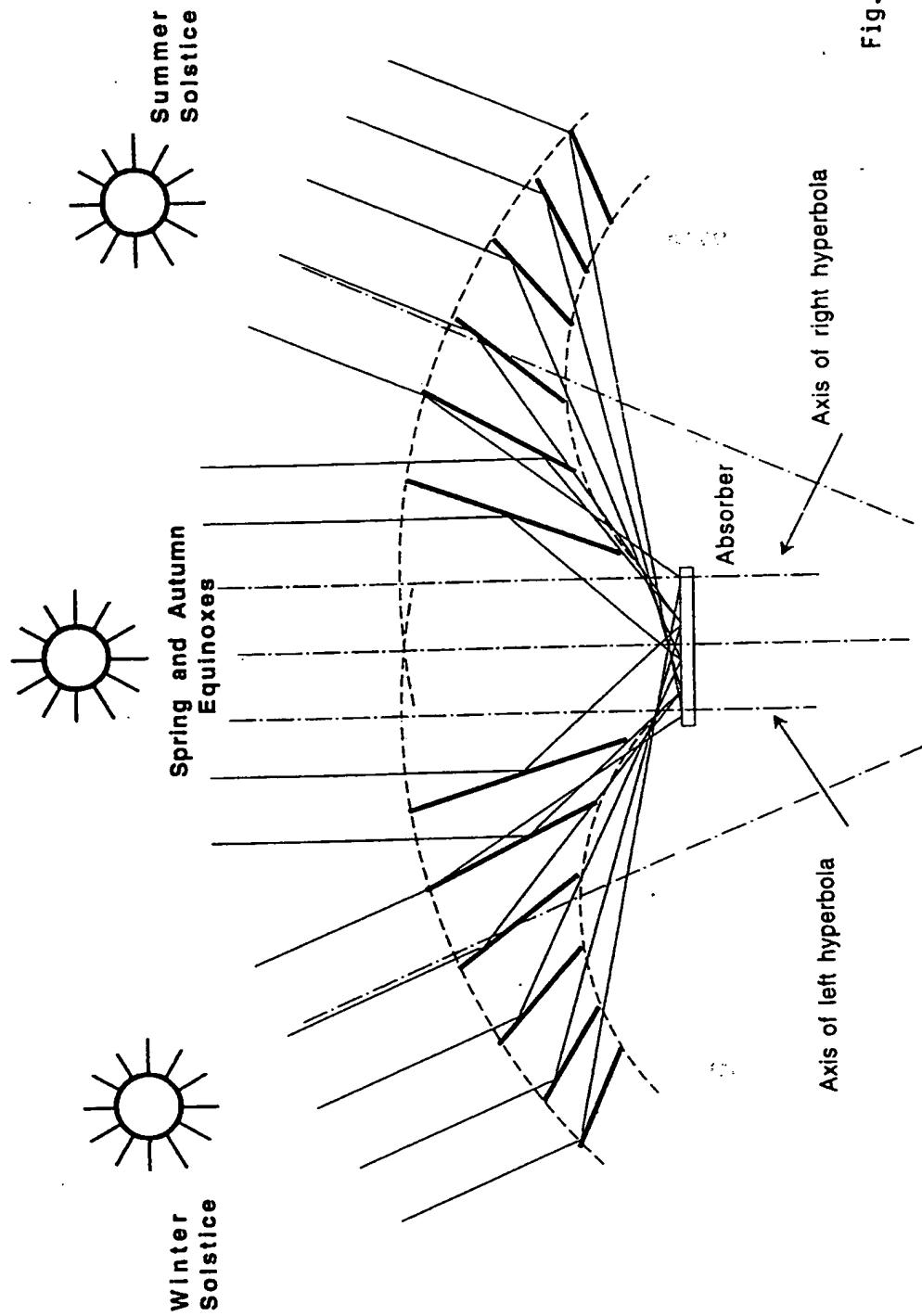


Fig. 11b

INTERNATIONAL SEARCH REPORT

International application No.

PCT/AU 95/00326

A. CLASSIFICATION OF SUBJECT MATTER

Int. Cl.⁶ G02B 17/00, 5/08, F24J 2/00, E04D 13/03, H01L 31/052

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC G02B 5/08, 17/00, 21/04, 23/02, 27/14, F24J 2/16, 3/02, F21V 7/05, E04D 13/03, G10K 11/28, 11/06.

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched
AU: IPC as above

Electronic data base consulted during the international search (name of data base, and where practicable, search terms used)

DERWENT : (ARRAY:OR SERIES) AND (REFLECT:OR MIRROR#) AND (FLAT OR PLANAR)

JAPIO : (ARRAY:OR SERIES) AND (REFLECT:OR MIRROR#) AND (FLAT OR PLANAR)

ENGINEERING INDEX ON CD-ROM: SOLAR AND CONCENTRAT: AND MIRROR # AND LINEAR:

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to Claim No.
X	WO 94/06046 A (THE AUSTRALIAN NATIONAL UNIVERSITY) 17 March 1994 figures 3-5, 17 and 18	1-4,7-10,12-15
X	US 4022186 A (NORTHROP, Jr.) 10 May 1977 whole document	1,2,4,7,8,11,15
X	WO 91/07681 A (MEMOTECH COMPUTERS LIMITED) 30 May 1991 figures 2-6	1,7-10

 Further documents are listed in the continuation of Box C. See patent family annex.

* Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance
 "E" earlier document but published on or after the international filing date
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 "O" document referring to an oral disclosure, use, exhibition or other means
 "P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
 "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
 "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
 "&" document member of the same patent family

Date of the actual completion of the international search 4 August 1995	Date of mailing of the international search report 17 AUGUST 1995
Name and mailing address of the ISA/AU AUSTRALIAN INDUSTRIAL PROPERTY ORGANISATION PO BOX 200 WODEN ACT 2606 AUSTRALIA Facsimile No. 06 2853929	Authorized officer  DEREK BARNES Telephone No. (06) 2832198

INTERNATIONAL SEARCH REPORT

International application No.

PCT/AU 95/00326

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate of the relevant passages	Relevant to Claim No.
X	FR 2382651 A (SAINT-POL) 29 September 1978 whole document	1-4,7,15

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No.

PCT/AU 95/00326

This Annex lists the known "A" publication level patent family members relating to the patent documents cited in the above-mentioned international search report. The Australian Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent Document Cited in Search Report	Patent Family Member				
WO 9406046	EP 663077				
WO 9107681	AU 70411/91	GB 8925482	GB	9021405	
END OF ANNEX					